Pakon TreDo / StaLa



European Technical Assessment (ETA-22/0910)

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European Technical Assessment ETA-22/0910 of 2023/03/28

I General Part

Technical Assessment Body issuing the ETA and designated according to Article 29 of the Regulation (EU) No 305/2011: ETA-Danmark A/S

Trade name of the construction product:

TreDo and StaLa Dowels

Product family to which the above construction product belongs:

Dowels for structural joints under static and quasi-static loading

Manufacturer:

Pakon AG Bahnhofstrasse 33 CH 8867 Niederurnen Internet www.pakonag.com

Manufacturing plant:

Pakon AG M 20 Areal, Wasterkingerweg CH 8193 Eglisau-Hüntwangen

This European Technical Assessment contains:

24 pages including 18 annexes which form an integral part of the document

This European Technical Assessment is issued in accordance with Regulation (EU) No 305/2011, on the basis of: EAD 050019-00-0301, Dowels for structural joints under static and quasi-static loading

This version replaces:

Pakon TreDo / StaLa

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II SPECIFIC PART OF THE EUROPEAN TECHNICAL ASSESSMENT

1 Technical description of the product

TreDo is a dowel system for structural joints between structural concrete elements, which is made up of a sound insulation box at one side and the dowel type DB-N at the other side of the structural joint. The dowel type DB-N consists of a circular steel sleeve and ancillary steel reinforcement welded on the backside of a rigid steel anchor plate. The sound insulation box is available in several design variants with regard to the support structure inside. For the "TreDo" version the circular steel bar is welded on a load distributing steel plate with an elastomeric bearing underneath. For the "TreDo Duo" version, the circular steel bar is welded between two load distributing steel plates, each with an elastomeric bearing underneath or respectively above. A load transfer is possible in vertical direction both up and down. Both variants are also available as twin versions with two separate elastomeric bearings, called "TreDo Twin" and "TreDo Twin Duo". For the "TreDo Duo+" version two additional steel plates with elastomeric bearings are attached laterally, so this version enables a load transfer in both vertical and horizontal directions. The support structures are surrounded by non-load bearing sound insulating material, all in all called sound insulation box. Furtheron there is the "TreDo ST" version with the steel bar resting on a vertical screw with height adjustment.

The TreDo steel bars are made of stainless steel or galvanized steel and the sleeves are made of stainless steel. Bars made of galvanized steel will be subjected to dry internal environment whereas bars and sleeves made of stainless steel can be subjected to environmental conditions acc. to EN 1993-1-4, Annex A depending on the corrosion resistance class.

The dowel system TreDo transmits shear forces across an expansion joint between structural concrete elements and rigid supports made of reinforced normal weight concrete of strength class C20/25 to C50/60 according to EN 206. The rigid support for the sound insulation box can also be a masonry wall with a concrete layer if necessary, whereas the bearing compressions at the masonry wall have to be designed acc. to EN 1996-1-1. The concrete elements are subjected to static and quasi-static actions only and they must have a minimum slab thickness of 150 mm. Further the concrete elements are subjected to fire exposure and designed acc. to EN 1992-1-1 and EN 1992-1-2.

TreDo belongs to the dowel family with a single bar and a sleeve with anchor plate and ancillary reinforcement. The dowel system allows axial movements only which take place at the circular sleeve.

StaLa is a dowel system for structural joints between a concrete member and a fixed point. StaLa uses the dowel types ESD-N and DB-N which consist of a circular dowel bar and a circular sleeve into which the bar is inserted at one side. At the other side a steel strap is welded to the head of the circular dowel bar and fixed mechanically to another concrete element or rigid member.

The StaLa steel bars are made of stainless steel, galvanized or normal steel and the sleeves are made of stainless steel or plastic. Bars made of galvanized or normal steel will be subjected to dry internal environment whereas bars and sleeves made of stainless steel or sleeves made of plastic can be subjected to environmental conditions acc. to EN 1993-1-4, Annex A depending on the corrosion resistance class.

The dowel system StaLa transmits shear loads across an expansion joint between a structural concrete element made of reinforced normal weight concrete of strength class C20/25 to C50/60 according to EN 206 and another rigid members. The concrete element and the rigid member are subjected to static and quasistatic actions only and the concrete elements must have a minimum slab thickness of 150 mm. Further the concrete element is subjected to fire exposure and designed acc. to EN 1992-1-1 and EN 1992-1-2.

StaLa belongs to the dowel family with a single bar and a sleeve with or without anchor plate and ancillary reinforcement. The dowel system allows axial movements only which take place at the circular sleeve. The fastening of the steel strap at a rigid member is supposed to be a fixed single bearing.

See further descriptions in Annex A.

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2 Specification of the intended use in accordance with the applicable EAD 330046-01-0602

The TreDo dowel system transmits shear loads across an expansion joint between a structural concrete element made of reinforced normal weight concrete of strength classes C20/25 to C50/60 according to EN 206 and another rigid support. This rigid support, where the sound insulation box is placed on, can be a concrete or masonry wall with a concrete layer if necessary.

The concrete element and the rigid supports are subjected to static and quasi-static actions only. They are subjected to fire exposure and have to be designed acc. to EN 1992-1-1 and EN 1992-1-2. The minimum concrete slab thickness is equal to $h_{\text{slab}} = \max (6 \cdot d_{\text{bar}}; 150 \text{ mm})$.

The TreDo dowel system uses the DB-N dowel type allowing axial movements only which take place at the circular sleeve.

Bars and load distribution steel plates made of galvanized steel will be subjected to dry internal environment. Bars, load distribution steel plates, anchor plates and sleeves made of stainless steel can be subjected to environmental conditions acc. to EN 1993-1-4, Annex A depending on the corrosion resistance class.

The StaLa dowel system also transmits shear loads across an expansion joint between a structural concrete element made of reinforced normal weight concrete of strength classes C20/25 to C50/60 according to EN 206 and another rigid member.

The concrete elements and the rigid members are subjected to static and quasi-static actions only. They are subjected to fire exposure and have to be designed acc. to EN 1992-1-1 and EN 1992-1-2. The minimum concrete slab thickness is equal to $h_{\text{slab}} = \max (6 \cdot d_{\text{bar}}; 150 \text{ mm})$.

The StaLa dowel system uses the ESD-N or DB-N dowel types allowing axial movements only which take place at the circular sleeves.

Bars, sleeves, anchor plates and steel straps made of galvanized or normal steel will be subjected to dry internal environment. Bars, steel strapes, anchor plates and sleeves made of stainless steel or plastic can be subjected to environmental conditions acc. to EN 1993-1-4, Annex A depending on the corrosion resistance class.

The performances given in Section 3 are only valid if the products are used in compliance with the specifications and conditions given in Annex A.

The provisions made in this European Technical Assessment are based on an assumed intended working life of the product of 50 years.

The indications given on the intended working life cannot be interpreted as a guarantee given by the producer or the Technical Assessment Body, but are to be regarded only as a means for selecting the appropriate products in relation to the expected economically reasonable working life of the works.

The real working life might be, in normal use conditions, considerably longer without major degradation affecting the basic requirements for construction works.

3 Performance of the product and references to the methods used for its assessment

Performances of the dowel systems, related to the basic requirements for construction works (hereinafter BWR), were determined according to EAD 050019-00-0301.

These performances, given in the following paragraphs, are valid as long as the components are the ones described in Annex A of this ETA.

Char	acteristic	Assessment of characteristic
3.1	Mechanical resistance and stability (BWR 1)
	Resistance to steel failure at ULS for TreDo with DB-N and StaLa with DB-N	e = 0 See Annex B1 to B2
	Resistance to steel failure at ULS for StaLa with ESD-N	e = 0.5 · d _{bar} See Annex B3 to B4
		X _{1,1} = 0.37
	Resistance to concrete edge failure at ULS	B _{spec,1} acc. to Annex B7
	for TreDo with DB-N and StaLa with DB-N	H _{spec,1} acc. to Annex B7
		$k_{1,1} = 0.5$
		$X_{1,1} = 0.60$
	Resistance to concrete edge failure at ULS	$B_{\text{spec},1} = 0$
	for StaLa with ESD-N	$H_{\text{spec},1} = c_1$ acc. to Annex B7
		$k_{1,1} = 0.5$
	Resistance to concrete edge failure at SLS for TreDo and StaLa with DB-N	$X_2 = 0.57$
	Resistance to concrete edge failure at SLS for StaLa with ESD-N	X ₂ = 0.41
3.2	Safety in case of fire (BWR2)	
	Reaction to fire	The dowels are made from steel classified as Euroclass A1 in accordance with EN 13501-1 and Commission Delegated Regulation 2016/364
	Resistance to fire	See Annex C1

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4 Attestation and verification of constancy of performance (AVCP)

4.1 AVCP system

According to the decision 1998/214/EC of the European Commission 1, as amended by 2003/639/EC, the system of assessment and verification of constancy of performance (see Annex V to Regulation (EU) No 305/2011) is:

2+

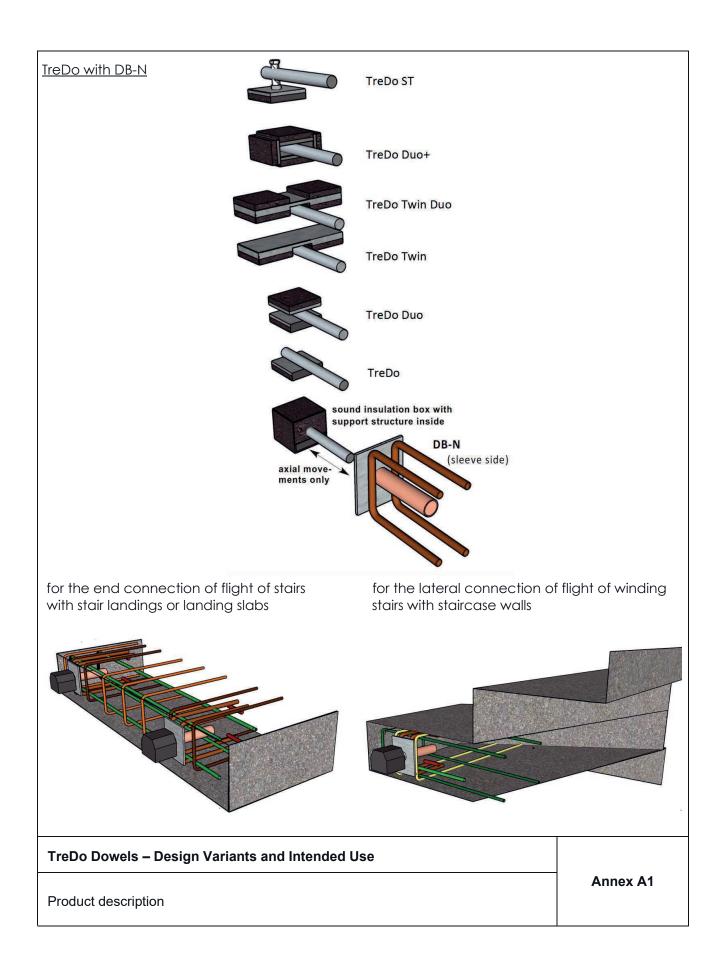
5 Technical details necessary for the implementation of the AVCP system, as foreseen in the applicable EAD

Technical details necessary for the implementation of the AVCP system are laid down in the control plan deposited at ETA-Danmark prior to CE marking.

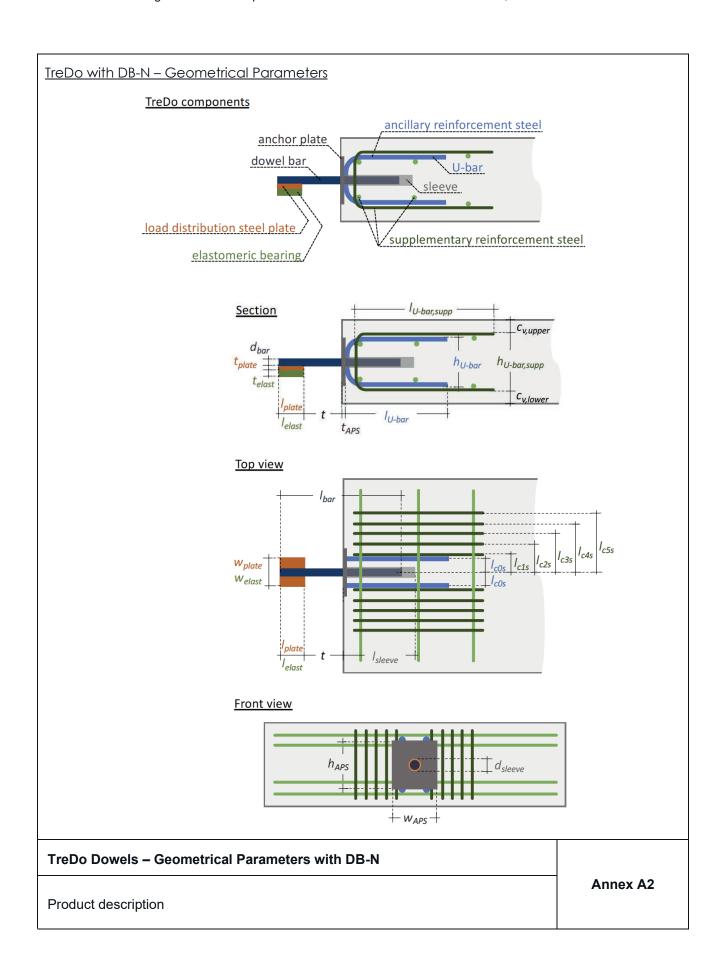
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Thomas Bruun

Managing Director, ETA-Danmark



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TreD	o Components	Dimensions	Material and Grades
	Bar	$d_{\text{bar}} = 27 \text{ mm}, 30 \text{ mm}, 33 \text{ mm}, 35 \text{ mm}, 40 \text{ mm}; $ $I_{\text{bar}} = 5 \cdot d_{\text{bar}} + \text{up to } 90 \text{ mm} + I_{\text{plate}}$ for joint widths 10-90 mm	Galvanized steel 1.7225, 1.7227 or stainless steel 1.4571, 1.4482, 1.4462, 1.4404, 1.4362 or 1.4301; all $R_{p0,2} \ge 460 \text{ N/mm}^2$
	Anchor plate*1)	w_{APS} = 65 mm up to 200 mm h_{APS} = 85 mm up to 210 mm t_{APS} = 4 mm up to 10 mm	Stainless steel 1.4571, 1.4482, 1.4462, 1.4404, 1.4307 or 1.4301; all $R_{p0,2} \ge 235 \text{ N/mm}^2$
N-80	Ancillary reinforcement steel *2 (welded on the anchor plate)	2 x 1 U-bar: Ø 12 mm, Ø 14 mm, Ø 16 mm or Ø 20 mm $I_{\text{U-bar}} \approx 0.3 \cdot \alpha_1 \cdot \alpha_4 \cdot I_{\text{b,rqd}} + 3 \text{Ø}_{\text{U-bar}}^{*4)}$ $I_{\text{U-bar}} \approx 5 \cdot d_{\text{bar}}$	B 500 A/B NR, B 500 A/B or B 550 A/B up to Ø 20 mm; Stainless steel 1.4571, 1.4482, 1.4462, 1.4404, 1.4362, 1.4301 up to Ø 20 mm; all $R_{p0,2} \ge 450 \text{ N/mm}^2$
	Supplementary reinforcement steel	2 x 1 up to 2 x 5 U-bars: Ø 12 mm, Ø 14 mm, Ø 16 mm, Ø 20 mm, Ø 25 mm or Ø 26 mm $I_{\text{U-bar,supp}} \approx 0.6 \cdot \alpha_1 \cdot \alpha_4 \cdot I_{\text{b,rqd}} + 3 \text{Ø}_{\text{U-bar,supp}}^{*4)}$ $I_{\text{U-bar,supp}} = I_{\text{slab}} - I_{\text{c,upper}} - I_{\text{c,upper}} - I_{\text{c,upper}}$	B 500 A/B or B 550 A/B
	Sleeve (circular)	$d_{\text{sleeve,in}} = d_{\text{bar}} + 1 \text{ mm}, t_{\text{sleeve}} \ge 1,5 \text{ mm}$ $l_{\text{sleeve}} = 5 \cdot d_{\text{bar}} + \text{up to } 95 \text{ mm}$	Stainless steel acc. to EN 1993-1-4 [5], R _{p0,2} ≥ 235 N/mm ²
Sound insulation box *3)	Load distribution steel plates	Steel plates for TreDo, TreDo ST and TreDo DUO: $W_{plate} = 70 \text{ mm}$ up to 180 mm $I_{plate} = 70 \text{ mm}$ up to 100 mm $t_{plate} \ge 5 \text{ mm}$ Steel plates laterally for TreDo DUO+: $W_{plate} = 50 \text{ mm}$ up to 70 mm $I_{plate} = 70 \text{ mm}$ up to 100 mm $t_{plate} \ge 5 \text{ mm}$	Galvanized steel, stainless steel or normal steel; R _{p0,2} ≥ 235 N/mm ²
Soul	Elastomeric bearings	$W_{elast} = 50 \text{ mm up to } 180 \text{ mm}$ $I_{elast} = 70 \text{ mm up to } 100 \text{ mm}$ $t_{elast} \ge 10 \text{ mm}$	EPDM or PUR

^{*1)} The height and width of the anchor plate can be increased slightly to meet the required thickness of concrete cover for the ancillary reinforcement steel.

The coefficient α_4 is usually set to 1.0. If there is a confinement by a transverse reinforcement bar with $\emptyset_t \ge 0.6 \cdot \emptyset_{U\text{-bar}, \text{supp}}$ welded to each leg of the supplementary reinforcement U-bars, the coefficient α_4 can be set to 0.7.

For the calculation of $\emph{I}_{b,rqd}$ the coefficient α_{ct} is set to 1.0.

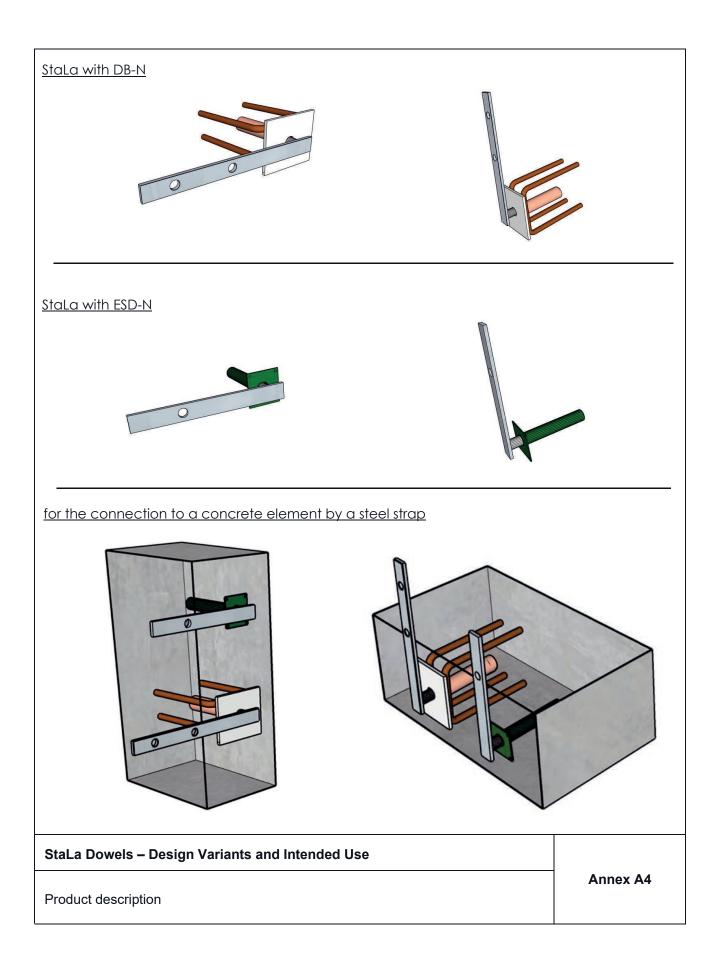
TreDo Dowels – Components with Dimensions, Materials and Grades	
Product description	Annex A3

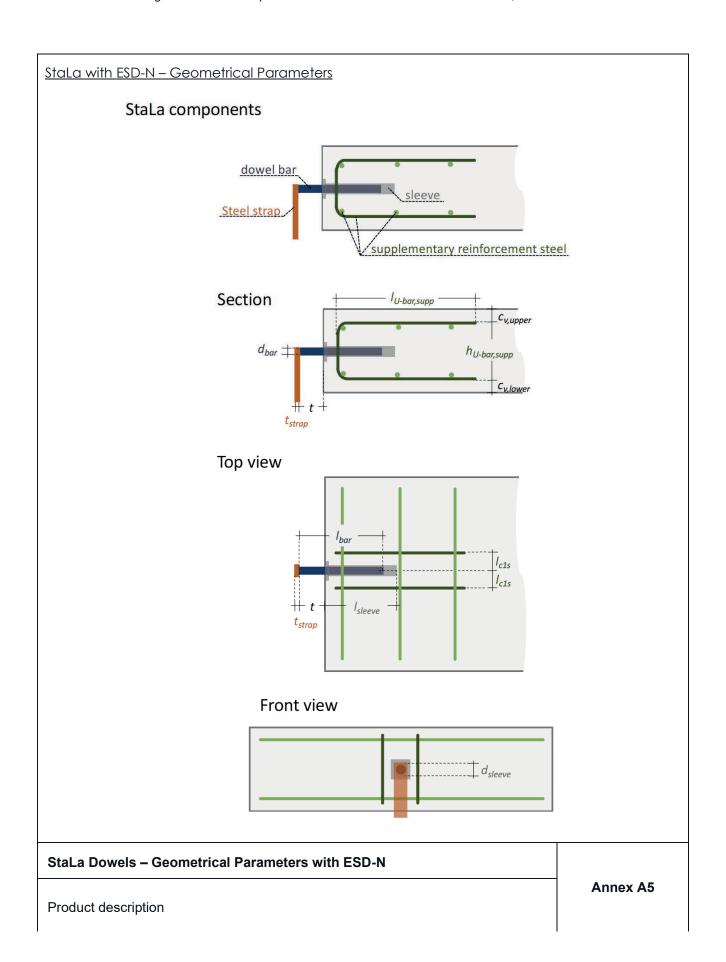
^{*2)} A normal reinforcing steel B 500 A/B can be used, if the thickness of the concrete cover in accordance with EN 1992-1-1 is fulfilled, which can be controlled, for example, by the dimensions of the anchor plate.

^{*3)} The sound insulation box with its support structures inside has to be designed following the Eurocodes and/or general type approvals

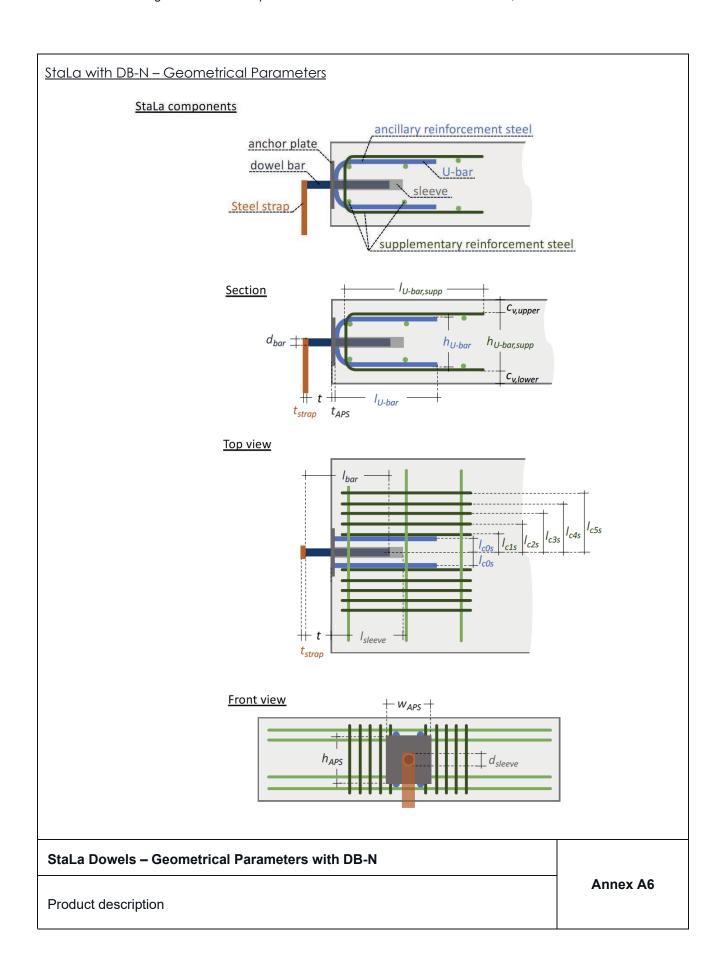
^{*4)} The coefficient α_1 is set to 1.0 for straight legs of the supplementary reinforcement U-bars. The coefficient α_1 is set to 0.7 for standard bends, standard hooks or standard loops at the end of the supplementary reinforcement U-bars.

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Stal	La Components	Dimensions	Material and Grades
	Bar	d_{bar} = 16 mm, 20 mm, 22 mm, 24 mm, 25 mm, 27 mm, 30 mm, 35 mm; I_{bar} = 5 · d_{bar} + up to 60 mm for joint widths 10-60 mm	Galvanized steel 1.7225, 1.7227 or stainless steel 1.4571, 1.4482, 1.4462, 1.4404, 1.4362 1.4301 or normal steel; all $R_{p0,2} \ge 235 \text{ N/mm}^2$
ESD-N	Supplementary reinforcement steel	2 x 1 U-bar: Ø 6 mm, Ø 8 mm, Ø 10 mm, Ø 12 mm, Ø 14 mm, Ø 16 mm, Ø 20 mm $I_{U\text{-bar},\text{supp}} = 0.6 \cdot \alpha_1 \cdot \alpha_4 \cdot I_{\text{b,rqd}} + 3 \mathcal{O}_{\text{U-bar},\text{supp}}^{*4}$ $h_{U\text{-bar},\text{supp}} = h_{\text{slab}} - c_{\text{v,upper}} - c_{\text{v,lower}}$	B 500 A/B or B 550 A/B
	Sleeve (circular)	$d_{\text{sleeve,in}} = d_{\text{bar}} + 1 \text{ mm}, t_{\text{sleeve}} \ge 1,5 \text{ mm}$ $I_{\text{sleeve}} = 5 \cdot d_{\text{bar}} + \text{up to 65 mm}$	Plastic PP, PE, PVC or stainless steel acc. to EN 1993-1-4 or normal steel; all $R_{p0,2} \ge 235 \text{ N/mm}^2$
	Bar	$d_{\text{bar}} = 20 \text{ mm}, 22 \text{ mm}, 24 \text{ mm}, 25 \text{ mm}, 27 \text{ mm}, 30 \text{ mm}, 35 \text{ mm}, 40 \text{ mm}; I_{\text{bar}} = 5 \cdot d_{\text{bar}} + \text{up to } 60 \text{ mm for joint}$ widths 10-60 mm and $I_{\text{bar}} = 5 \cdot d_{\text{bar}} + \text{up to}$ 120 mm for joint widths 61-120 mm	Galvanized steel 1.7225, 1.7227 or stainless steel 1.4571, 1.4482, 1.4462, 1.4404, 1.4362, 1.4301 or normal steel; all $R_{p0,2} \ge 460 \text{ N/mm}^2$
	Anchor plate*1)	w_{APS} = 65 mm up to 200 mm h_{APS} = 85 mm up to 210 mm t_{APS} = 4 mm up to 10 mm	Stainless steel 1.4571, 1.4482, 1.4462, 1.4404, 1.4307, 1.4301 or normal steel; all $R_{p0,2} \ge 235 \text{ N/mm}^2$
N-80	Ancillary reinforcement steel *2) (welded on the anchor plate)	2 x 1 U-bar: Ø 10 mm, Ø 12 mm, Ø 14 mm, Ø 16 mm or Ø 20 mm $I_{\text{U-bar}} \approx 0.3 \cdot \alpha_1 \cdot \alpha_4 \cdot I_{\text{b,rqd}} + 3 \text{Ø}_{\text{U-bar}}^{*4}$ $h_{\text{U-bar}} \approx 5 \cdot d_{\text{bar}}$	B 500 A/B NR, B 500 A/B or B 550 A/B up to Ø 20 mm; Stainless steel 1.4571, 1.4482, 1.4462, 1.4404, 1.4362, 1.4301 up to Ø 20 mm; all $R_{p0.2} \ge 450 \text{ N/mm}^2$
	Supplementary reinforcement steel	2 x 1 up to 2 x 5 U-bars: Ø 10 mm, Ø 12 mm, Ø 14 mm, Ø 16 mm, Ø 20 mm, Ø 25 mm or Ø 26 mm $I_{\text{U-bar,supp}} \approx 0.6 \cdot \alpha_1 \cdot \alpha_4 \cdot I_{\text{b,rqd}} + 3 \text{Ø}_{\text{U-bar,supp}}^{*4}$ $I_{\text{U-bar,supp}} = I_{\text{slab}} - C_{\text{v,upper}} - C_{\text{v,lower}}$	B 500 A/B or B 550 A/B
	Sleeve (circular)	$d_{\text{sleeve,in}} = d_{\text{bar}} + 1 \text{ mm}, t \ge 1,5 \text{ mm}$ $I_{\text{sleeve}} = 5 \cdot d_{\text{bar}} + \text{up to 65 mm}$	Stainless steel acc. to EN 1993-1-4 or normal steel; all R _{p0,2} ≥ 235 N/mm ²
Strap	Steel strap *3)	dimensions can be chosen individually	Galvanized steel, stainless steel or normal steel; R _{p0,2} ≥ 235 N/mm ²

^{*1)} The height and width of the anchor plate can be increased slightly to meet the required thickness of concrete cover for the ancillary reinforcement steel.

For the calculation of $I_{b,rqd}$ the coefficient α_{ct} is set to 1.0.

StaLa Dowels – Components with Dimensions, Materials and Grades	
Product description	Annex A7

^{*2)} A normal reinforcing steel B 500 A/B can be used, if the thickness of the concrete cover in accordance with EN 1992-1-1 is fulfilled, which can be controlled, for example, by the dimensions of the anchor plate.

^{*3)} The steel strap with its fixing to the dowel bar and the other rigid support has to be designed following the Eurocodes

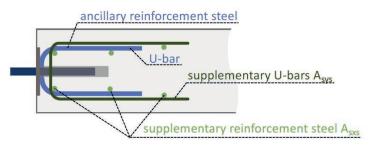
^{*4)} The coefficient α₁ is set to 1.0 for straight legs of the supplementary reinforcement U-bars. The coefficient α₁ is set to 0.7 for standard bends, standard hooks or standard loops at the end of the supplementary reinforcement U-bars.

The coefficient α₄ is usually set to 1.0. If there is a confinement by a transverse reinforcement bar with Ø₁ ≥ 0.6 · Ø∪-bar,supp welded to each leg of the supplementary reinforcement U-bars, the coefficient α₄ can be set to 0.7.

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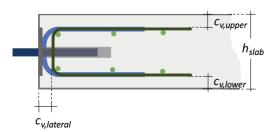
<u>TreDo and StaLa with DB-N – Arrangement of Supplementary Reinforcement Steel</u>

Designation of components



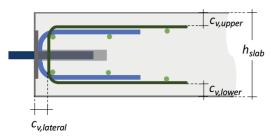
 $A_{sxs} \ge 2x 3\emptyset A_{sys}$ and A_{sys} acc. to Annex B5

Arrangement of supplementary reinforcement steel at small slab thicknesses

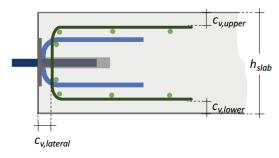


The minimum slab thickness is: min $h_{\text{slab}} = h_{\text{U-bar}} + c_{\text{v,upper}} + c_{\text{v,lower}}$ $\geq \max \left(6 \cdot d_{\text{bar}}; 150 \text{ mm}\right)$ with $h_{\text{U-bar}}$ acc. to Annex B7

Arrangement of supplementary reinforcement steel at average slab thicknesses



Arrangement of supplementary reinforcement steel at greater slab thicknesses



TreDo and StaLa Dowels with DB-N – Arrangement of Reinforcement Steel	
Product description	Annex A8

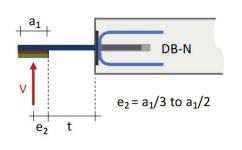
<u>TreDo and StaLa with DB-N – Arrangement of Reinforcement Steel Bars</u> Designation of components supplementary reinforcement steel A $A_{sxs} = 2 \emptyset_{U-bar}$ ancillary reinforcement steel beam stirrups respectively wall reinforcement layers Arrangement of ancillary and supplementary reinforcement steel bars at beams The minimum width of the beam is: $min w_{beam} = t_{APS} + t_{U-bar} + c_v$ with t_{APS} and l_{U-bar} acc. to Annexes A3 and A7 $w_{\rm beam}$ W_{beam} W_{beam} Arrangement of ancillary and supplementary reinforcement steel bars at walls The minimum wall thickness is: $\min t_{\text{wall}} = t_{\text{APS}} + I_{\text{U-bar}} + c_{\text{V}}$ with t_{APS} and l_{U-bar} acc. to Annexes A3 and A7 twall TreDo and StaLa Dowels with DB-N - Arrangement of Reinforcement Steel Annex A9 Product description

<u>Fire Protection Collars for TreDo and StaLa</u> Material and dimensions 2 mm mineral wool intumescent plate 160 mm up to 120 mm **Fire Protection Collars** Annex A10 Product description

TreDo ST

TreDo Duo+

TreDo With DB-N TreDo Twin TreDo Duo TreDo TreDo



Note 1: For TreDo ST the distance to the point of the hinged support is $e_2 = a_1/2$, whereas for all other variants the distance can be chosen to $e_2 = a_1/3$ up to $e_2 = a_1/2$.

Note 2: In case of two-directional forces acting perpendicular to the dowel axis the shear force $V_{\text{Ed,s}}$ has to be determined as resultant force.

TreDo with DB-N, dowel bar $R_{p0,2} = 750 \text{ N/mm}^2$

V _{Rd,s,ULS} [kN]		joint width plus partial support width $t + e_2$ [mm]													
		30	40	50	60	70	80	90	100	110	120				
	Ø 27	67,1	50,3	40,3	33,6	28,8	25,2	22,4	20,1	18,3	16,8				
[mm]	Ø 30	92,0	69,0	55,2	46,0	39,4	34,5	30,7	27,6	25,1	23,0				
	Ø 33	122,5	91,9	73,5	61,3	52,5	45,9	40,8	36,8	33,4	30,6				
d bar	Ø 35	146,2	109,6	87,7	73,1	62,6	54,8	48,7	43,8	39,9	36,5				
	Ø 40	218,2	163,6	130,9	109,1	93,5	81,8	72,7	65,5	59,5	54,5				

TreDo with DB-N, dowel bar $R_{p0,2} = 690 \text{ N/mm}^2$

V _{Rd,s,ULS} [kN]		joint width plus partial support width $t + e_2$ [mm]													
		30	40	50	60	70	80	90	100	110	120				
	Ø 27	61,7	46,3	37,0	30,9	26,5	23,1	20,6	18,5	16,8	15,4				
[mm]	Ø 30	84,7	63,5	50,8	42,3	36,3	31,8	28,2	25,4	23,1	21,2				
	Ø 33	112,7	84,5	67,6	56,4	48,3	42,3	37,6	33,8	30,7	28,2				
d bar	Ø 35	134,5	100,9	80,7	67,2	57,6	50,4	44,8	40,3	36,7	33,6				
	Ø 40	200,7	150,5	120,4	100,4	86,0	75,3	66,9	60,2	54,7	50,2				

TreDo with DB-N, dowel bar $R_{p0,2} = 460 \text{ N/mm}^2$

V _{Rd,s,ULS} [kN]		joint width plus partial support width $t + e_2$ [mm]													
		30	40	50	60	70	80	90	100	110	120				
	Ø 27	41,2	30,9	24,7	20,6	17,6	15,4	13,7	12,3	11,2	10,3				
[mm]	Ø 30	56,5	42,3	33,9	28,2	24,2	21,2	18,8	16,9	15,4	14,1				
	Ø 33	75,1	56,4	45,1	37,6	32,2	28,2	25,0	22,5	20,5	18,8				
d bar	Ø 35	89,6	67,2	53,8	44,8	38,4	33,6	29,9	26,9	24,4	22,4				
	Ø 40	133,8	100,4	80,3	66,9	57,4	50,2	44,6	40,1	36,5	33,5				

TreDo with DB-N - Resistances to Steel Failure

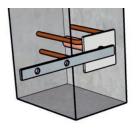
Performances

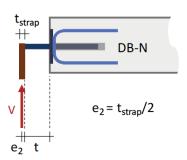
Annex B1

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StaLa with DB-N







StaLa with DB-N, dowel bar $R_{p0,2} = 750 \text{ N/mm}^2$

V _{Rd,s,ULS} [kN]			joint width plus partial support width $t + e_2$ [mm]													
		10	20	30	40	50	60	70	80	90	100	110	120			
	Ø 20	73,4	40,9	27,3	20,5	16,4	13,6	11,7	10,2	9,1	8,2	7,4	6,8			
	Ø 22	93,0	54,5	36,3	27,2	21,8	18,2	15,6	13,6	12,1	10,9	9,9	9,1			
<u>ر</u>	Ø 24	114,9	70,7	47,1	35,3	28,3	23,6	20,2	17,7	15,7	14,1	12,9	11,8			
[mm]	Ø 25	126,6	79,9	53,3	40,0	32,0	26,6	22,8	20,0	17,8	16,0	14,5	13,3			
bar	Ø 27	151,7	100,7	67,1	50,3	40,3	33,6	28,8	25,2	22,4	20,1	18,3	16,8			
p	Ø 30	193,6	136,9	92,0	69,0	55,2	46,0	39,4	34,5	30,7	27,6	25,1	23,0			
	Ø 35	274,6	208,4	146,2	109,6	87,7	73,1	62,6	54,8	48,7	43,8	39,9	36,5			
	Ø 40	369,5	293,8	218,2	163,6	130,9	109,1	93,5	81,8	72,7	65,5	59,5	54,5			

StaLa with DB-N, dowel bar $R_{p0,2}$ = 690 N/mm²

W	[LAJ]	joint width plus partial support width $t + e_2$ [mm]											
V _{Rd,s,ULS} [kN]		10	20	30	40	50	60	70	80	90	100	110	120
	Ø 20	67,6	37,6	25,1	18,8	15,1	12,5	10,8	9,4	8,4	7,5	6,8	6,3
	Ø 22	85,6	50,1	33,4	25,0	20,0	16,7	14,3	12,5	11,1	10,0	9,1	8,3
드	Ø 24	105,7	65,0	43,4	32,5	26,0	21,7	18,6	16,3	14,5	13,0	11,8	10,8
[mm]	Ø 25	116,5	73,5	49,0	36,8	29,4	24,5	21,0	18,4	16,3	14,7	13,4	12,3
bar	Ø 27	139,6	92,6	61,7	46,3	37,0	30,9	26,5	23,1	20,6	18,5	16,8	15,4
р	Ø 30	178,2	125,9	84,7	63,5	50,8	42,3	36,3	31,8	28,2	25,4	23,1	21,2
	Ø 35	252,6	191,7	134,5	100,9	80,7	67,2	57,6	50,4	44,8	40,3	36,7	33,6
	Ø 40	339,9	270,3	200,7	150,5	120,4	100,4	86,0	75,3	66,9	60,2	54,7	50,2

StaLa with DB-N, dowel bar $R_{p0,2}$ = 460 N/mm²

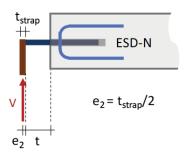
V _{Rd,s,ULS} [kN]			joint width plus partial support width $t + e_2$ [mm]												
		10	20	30	40	50	60	70	80	90	100	110	120		
	Ø 20	45,0	25,1	16,7	12,5	10,0	8,4	7,2	6,3	5,6	5,0	4,6	4,2		
	Ø 22	57,1	33,4	22,3	16,7	13,4	11,1	9,5	8,3	7,4	6,7	6,1	5,6		
교	Ø 24	70,4	43,4	28,9	21,7	17,3	14,5	12,4	10,8	9,6	8,7	7,9	7,2		
[mm]	Ø 25	77,6	49,0	32,7	24,5	19,6	16,3	14,0	12,3	10,9	9,8	8,9	8,2		
bar	Ø 27	93,1	61,7	41,2	30,9	24,7	20,6	17,6	15,4	13,7	12,3	11,2	10,3		
р	Ø 30	118,8	83,9	56,5	42,3	33,9	28,2	24,2	21,2	18,8	16,9	15,4	14,1		
	Ø 35	168,4	127,8	89,6	67,2	53,8	44,8	38,4	33,6	29,9	26,9	24,4	22,4		
	Ø 40	226,6	180,2	133,8	100,4	80,3	66,9	57,4	50,2	44,6	40,1	36,5	33,5		

StaLa with DB-N – Resistances to Steel Failure	
Performances	Annex B2

StaLa with ESD-N







StaLa with ESD-N, dowel bar $R_{p0,2} = 750 \text{ N/mm}^2$

\/	[[AJ]]	joint	joint width plus partial support width $t + e_2$ [mm]								
V _{Rd}	,s,ULS [kN]	10	20	30	40	50	60				
	Ø 16	23,3	15,0	11,0	8,7	7,2	6,2				
	Ø 20	40,9	27,3	20,5	16,4	13,6	11,7				
ᆮ	Ø 22	51,9	35,1	26,6	21,4	17,9	15,3				
[mm]	Ø 24	64,3	44,2	33,7	27,2	22,8	19,6				
bar	Ø 25	71,0	49,2	37,6	30,4	25,6	22,0				
р	Ø 27	85,7	60,1	46,3	37,6	31,7	27,4				
	Ø 30	110,5	78,9	61,4	50,2	42,5	36,8				
	Ø 35	159,5	116,9	92,3	76,3	65,0	56,6				

StaLa with ESD-N, dowel bar $R_{p0,2}$ = 690 N/mm²

V _{Rd.s.ULS} [kN]		joint	joint width plus partial support width $t + e_2$ [mm]									
V Rd	s,ULS [KIN]	10	20	30	40	50	60					
	Ø 16	21,4	13,8	10,1	8,0	6,6	5,7					
	Ø 20	37,6	25,1	18,8	15,1	12,5	10,8					
ᆮ	Ø 22	47,7	32,3	24,4	19,6	16,4	14,1					
[mm]	Ø 24	59,1	40,6	31,0	25,0	21,0	18,1					
bar	Ø 25	65,3	45,2	34,6	28,0	23,5	20,3					
р	Ø 27	78,8	55,3	42,6	34,6	29,2	25,2					
	Ø 30	101,6	72,6	56,5	46,2	39,1	33,9					
	Ø 35	146,7	107,6	84,9	70,2	59,8	52,1					

StaLa with ESD-N, dowel bar $R_{p0,2}$ = 460 N/mm²

V _{Rd,s,ULS} [kN]		joint	joint width plus partial support width $t + e_2$ [mm]								
V Rd	s,ULS [KIN]	10	20	30	40	50	60				
	Ø 16	14,3	9,2	6,8	5,4	4,4	3,8				
	Ø 20	25,1	16,7	12,5	10,0	8,4	7,2				
ᆫ	Ø 22	31,8	21,5	16,3	13,1	10,9	9,4				
[mm]	Ø 24	39,4	27,1	20,6	16,7	14,0	12,0				
bar	Ø 25	43,6	30,2	23,1	18,7	15,7	13,5				
р	Ø 27	52,5	36,9	28,4	23,1	19,4	16,8				
	Ø 30	67,7	48,4	37,6	30,8	26,1	22,6				
	Ø 35	97,8	71,7	56,6	46,8	39,8	34,7				

Stal a with	FSD-N -	 Resistances to 	Steel Failure
Stala With	E3D-I1 -	' NESISIAIILES แ	J Steel Fallule

Performances

Annex B3

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StaLa with ESD-N (continued)

StaLa with ESD-N, dowel bar $R_{p0,2} = 355 \text{ N/mm}^2$

V _{Rd,s,ULS} [kN]		joint	joint width plus partial support width $t + e_2$ [mm]									
V Rd	s,ULS [KIN]	10	20	30	40	50	60					
	Ø 16	11,0	7,1	5,2	4,1	3,4	2,9					
	Ø 20	19,4	12,9	9,7	7,7	6,5	5,5					
ᆮ	Ø 22	24,5	16,6	12,6	10,1	8,5	7,3					
[mm]	Ø 24	30,4	20,9	15,9	12,9	10,8	9,3					
bar	Ø 25	33,6	23,3	17,8	14,4	12,1	10,4					
р	Ø 27	40,5	28,4	21,9	17,8	15,0	13,0					
	Ø 30	52,3	37,3	29,0	23,8	20,1	17,4					
	Ø 35	75,5	55,3	43,7	36,1	30,7	26,8					

StaLa with ESD-N, dowel bar $R_{p0,2}$ = 275 N/mm²

W.	[[AN]]	joint width plus partial support width $t + e_2$ [mm]									
V Rd	,s,ULS [kN]	10	20	30	40	50	60				
	Ø 16	8,5	5,5	4,0	3,2	2,6	2,3				
	Ø 20	15,0	10,0	7,5	6,0	5,0	4,3				
드	Ø 22	19,0	12,9	9,7	7,8	6,5	5,6				
[mm]	Ø 24	23,6	16,2	12,3	10,0	8,4	7,2				
bar	Ø 25	26,0	18,0	13,8	11,2	9,4	8,1				
р	Ø 27	31,4	22,0	17,0	13,8	11,6	10,0				
	Ø 30	40,5	28,9	22,5	18,4	15,6	13,5				
	Ø 35	58,5	42,9	33,8	28,0	23,8	20,7				

StaLa with ESD-N, dowel bar $R_{p0,2}$ = 235 N/mm²

\/	[[NJ]	joint	joint width plus partial support width $t + e_2$ [mm]									
V Rd	,s,ULS [kN]	10	20	30	40	50	60					
	Ø 16	7,3	4,7	3,5	2,7	2,3	1,9					
	Ø 20	12,8	8,5	6,4	5,1	4,3	3,7					
ᆮ	Ø 22	16,2	11,0	8,3	6,7	5,6	4,8					
[mm]	Ø 24	20,1	13,8	10,5	8,5	7,1	6,2					
d bar	Ø 25	22,3	15,4	11,8	9,5	8,0	6,9					
р	Ø 27	26,8	18,8	14,5	11,8	9,9	8,6					
	Ø 30	34,6	24,7	19,2	15,7	13,3	11,5					
	Ø 35	50,0	36,6	28,9	23,9	20,4	17,7					

StaLa with ESD-N – Resistances to Steel Failure (continued)	
Performances	Annex B4

Resistances to Concrete Edge Failure

The characteristic resistance to concrete edge failure of the slab at ULS is calculated following EOTA TR065, chapter 2.4, whereas equation (5a) is supplemented by the statical reduction factor k_{stat} .

$$\begin{split} V_{Rk,ce,ULS} &= V_{Rk,ce,1} + V_{Rk,ce,2} \\ V_{Rk,ce,1} &= X_1 \cdot k_{stat} \cdot \sum \psi_i \cdot A_s \cdot f_{yk} \cdot \left(\frac{f_{ck}}{f_{ck,nom}}\right)^{k_1} \\ \psi_i &= 1 - 0.2 \cdot \left(\frac{l_{c,i}}{c_1}\right) \quad ; \quad f_{ck,nom} = 20 \ N/mm^2 \end{split}$$

$$\begin{split} V_{Rk,ce,2} &= \pi \cdot d_s \cdot \sum {l'}_{1,i} \cdot 2.25 \cdot 0.7 \cdot 0.3 \cdot f_{ck}^{2/3} \\ & l'_{1,i} = l_{1,i} - l_{1,min} \\ & l_{1,min} = d_s + 0.5 \cdot d_b \qquad \text{with} \qquad d_b \geq 4 \cdot d_s \end{split}$$

The characteristic resistance to concrete edge failure of the slab at SLS is calculated acc. to EOTA TR065, chapter 2.5.

$$V_{Rk,ce,SLS} = X_2 \cdot V_{Rk,ce,ULS}$$

In accordance with EOTA TR065 [2], chapters 2.2, 2.4 and 2.5 the design values of the resistances to concrete edge failure of the slab are:

$$V_{Rd,ce,ULS} = rac{V_{Rk,ce,ULS}}{\gamma_{m,ce,ULS}}$$
 $\gamma_{m,ce,ULS} = 1.5$ partial safety factor

$$V_{Rd,ce,SLS} = rac{V_{Rk,ce,SLS}}{\gamma_{m,ce,SLS}}$$
 $\gamma_{m,ce,SLS} = 1.0$ partial safety factor

Resistances to Concrete Edge Failure – Design Equations	
Performances	Annex B5

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Resistances to Concrete Edge Failure (continued)

Statical reduction factor k_{stat} for TreDo with DB-N and StaLa with DB-N

k stat		joint width plus partial support width $t + e_2$ [mm]										
dowel bar	10	20	30	40	50	60	70	80	90	100	110	120
Ø 20 mm	0,92	0,78	0,68	0,61	0,55	0,50	0,45	0,42	0,39	0,36	0,34	0,32
Ø 30 mm	0,94	0,84	0,76	0,69	0,64	0,59	0,55	0,51	0,48	0,45	0,43	0,41
Ø 40 mm	0,95	0,87	0,80	0,75	0,70	0,65	0,61	0,58	0,55	0,52	0,49	0,47

Note 1: For intermediate dowel bar diameters a linear interpolation is possible.

Note 2: For TreDo with DB-N a sum of $t + e_2$ from 30 mm to 120 mm is applicable and for StaLa with DB-N a sum of $t + e_2$ from 10 mm to 120 mm is possible. For the definition of $t + e_2$ see Annexes B1 to B4.

Alternatively the statical reduction factor k_{stat} for TreDo with DB-N and StaLa with DB-N can be calculated under consideration of $t + e_2$ (see Annexes B1 to B4)

- for all dowel bar sizes from Ø 20 mm or greater to:

$$k_{stat} = -0.249 \cdot \ln(t + e_2) + 1.51$$

- for dowel bar sizes from Ø 30 mm or greater to:

$$k_{stat} = -0.225 \cdot \ln(t + e_2) + 1.50$$

with a sum of $t + e_2$ from 30 mm to 120 mm for TreDo with DB-N and a sum of $t + e_2$ from 10 mm to 120 mm for StaLa with DB-N

Statical reduction factor k_{stat} for StaLa with ESD-N

k _{stat}	joint w	joint width plus partial support width $t + e_2$ [mm]								
dowel bar	10	10 20 30 40 50 60								
Ø 16 mm	0,91	0,77	0,67	0,60	0,53	0,48				
Ø 25 mm	0,93	0,82	0,73	0,66	0,60	0,55				
Ø 35 mm	0,94	0,85	0,77	0,71	0,65	0,60				

Note 1: For intermediate dowel bar diameters a linear interpolation is possible.

Alternatively the statical reduction factor k_{stat} for StaLa with ESD-N can be calculated under consideration of $t + e_2$ (see Annexes B1 to B4)

– for all dowel bar sizes from Ø 16 mm or greater to:

$$k_{stat,StaLa} = \frac{(t+e_2)^2}{10.000} - \frac{16 \cdot (t+e_2)}{1.000} + 1,06$$

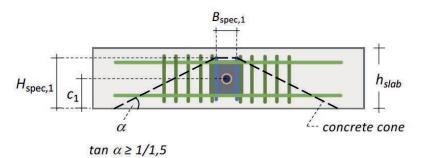
– for dowel bar sizes from Ø 25 mm or greater to:

$$k_{stat,StaLa} = \frac{8 \cdot (t + e_2)^2}{100.000} - \frac{13 \cdot (t + e_2)}{1.000} + 1,05$$

with a sum of $t + e_2$ from 10 mm to 60 mm for StaLa with ESD-N

Resistances to Concrete Edge Failure (continued) – Statical Reduction Factor	
Performances	Annex B6

Resistances to Concrete Edge Failure (continued)



TreDo with DB-N – Design parameters

Dowel name	DB-N 27	DB-N 30	DB-N 33	DB-N 35	DB-N 40
d _{bar} [mm]	27	30	33	35	40
U-bars [mm]	2Ø12	2Ø14	2Ø16	2Ø16	2 Ø20
hu-bar [mm]	140	140	160	170	210
Icos [mm]	26,5	29,5	33	34,5	40
B _{spec,1} [mm]	53	59	66	69	80
H _{spec,1} [mm]	C1+64	C1+68	c ₁ +72	C1+77	C1+95

StaLa with DB-N – Design parameters

Dowel name	DB-N 20	DB-N 22	DB-N 24 DB-N 25	DB-N 27	DB-N 30	DB-N 35	DB-N 40
d _{bar} [mm]	20	22	24/25	27	30	35	40
U-bars [mm]	2Ø10	2Ø10	2Ø12	2Ø12	2Ø14	2Ø16	2 Ø20
hu-bar [mm]	100	100	120	140	150	170	210
I _{c0s} [mm]	21	22	25	26,5	29,5	34,5	40
B _{spec,1} [mm]	42	44	50	53	59	69	80
Hspec,1 [mm]	C1+45	C1+45	C1+54	C1+64	C1+68	C1+77	C1+95

For StaLa with ESD-N the design parameters are in general:

 $B_{\text{spec},1} = 0$

 $H_{\text{spec},1} = C_1$

Resistances to Concrete Edge Failure (continued) – Design Parameters	
Performances	Annex B7

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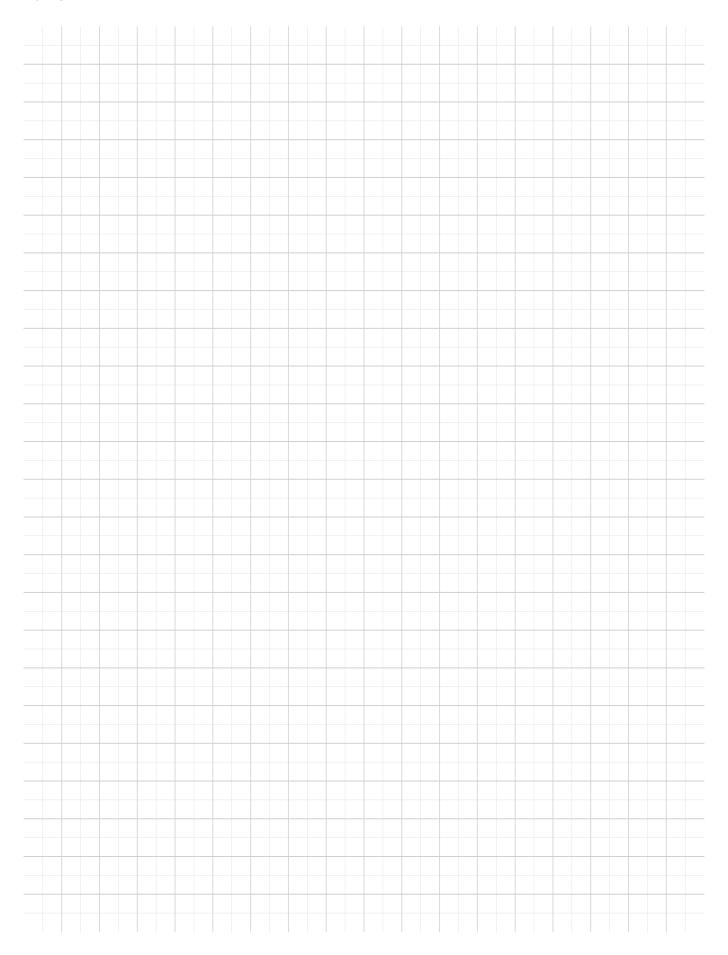
Performance characteristics with regard to load-bearing performance in case of fire

If the performance characteristics specified in Section 3 are complied with, the load-bearing capacity of the connection of reinforced concrete members with the shear force dowel in accordance with the intended use is also given under fire exposure according to the standard temperature curve for a duration of 120 minutes if the following conditions are met:

- Compliance with the design conditions in accordance with Annex A and the design requirements according to Annex B.
- Use and installation in accordance with Annex A and B.
- The design of the load-bearing capacity of the connection with the shear force dowel under normal temperatures was carried out in accordance with EOTA TR 065 and Annex B.
- For structural fire design (accidental fire situation), the action shall be determined on the basis of the normal temperature design of the load-bearing capacity, using a maximum reduction coefficient $\eta_{\rm fi}$ in accordance with EN 1992-1-2 or EN 1993-1-2 respectively, Section 2.4.2 of $\eta_{\rm fi}$ = 0,7.
- The load-bearing capacity of the reinforced concrete members under fire exposure shall be verified for the intended use.
- The required axis distances of the steel reinforcement bars in case of fire have to be considered in accordance with EN 1992-1-2. The resulting concrete covers $c_{\rm v}$ and the minimum slab thickness $h_{\rm slab}$ acc. to Annex A8 and the minimum beam widths $w_{\rm beam}$ or wall thicknesses $t_{\rm wall}$ acc. to Annex A9 have to be met.

TreDo and StaLa Dowels – Performance Characteristics in Case of Fire	
Resistance to fire	Annex C1

NOTES





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